

1 **HOW DO ROUNDABOUT ENTRY DESIGN PARAMETERS INFLUENCE SAFETY?**

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1 ABSTRACT

2 Roundabout is considered the safest intersection design; however, its safety effect may not be
3 satisfactory at each specific roundabout. This is true especially in countries where roundabout
4 design is a relatively new concept, such as in the Czech Republic. Specifically, most Czech
5 roundabout crashes were found to occur on entries. This motivated the presented study to
6 answer the question, how do entry design parameters influence safety on Czech roundabouts,
7 and if possible, use the findings to update current Czech roundabout design guidelines. To this
8 end, the study comprised three analyses: crash-based safety performance functions, speed
9 analysis, and finally safety performance functions which incorporated speed. All three analyses
10 proved that entry design parameters have a statistically significant influence on safety, in terms
11 of crash frequency, severity and speeds. Given the study objective, this fact should be
12 considered in Czech roundabout design guidelines.

1 INTRODUCTION

2 Intersections, where road users may change their directions in order to get to their destinations,
3 are crucial for the road network operation. However, they also present a discontinuity in the
4 road network and, therefore, a potential hazard, due to a number of conflict points and traffic
5 complexity (1 – 4). In the United States, more than 50% of fatal and injury crashes take place
6 at or near intersections (5). In Europe, every 5th road fatality is due to intersection crashes (6).
7 In this context, roundabout is considered the safest intersection design, as it introduces few
8 conflict points and low speeds, which are associated with reduction of number and severity of
9 crashes (7). Nevertheless, the safety improvements may not produce satisfactory results at each
10 specific roundabout (8); in addition, the crash reductions are most pronounced for motor
11 vehicles and less pronounced for pedestrians or bicyclists (9). Other roundabout disadvantages
12 comprise for example difficulties for visually impaired users, or potential increase of single-
13 vehicle and fixed-object crashes (10).

14 One of explanations, offered by Montella (11), is that there may be safety issues
15 especially in countries where roundabout design is a relatively new concept. The Czech
16 Republic, where roundabouts have emerged since early 2000s, may be one of such examples.
17 In fact, Czech roundabout safety performance was found inferior, compared to other European
18 countries (12), which may be due to insufficient roundabout experience, both in terms of design
19 practice and driving performance. Similarly to other countries (9), most Czech roundabout
20 crashes occur on entries: entering-circulating crashes present 58% of all roundabout crashes
21 (13), probably due to failure to give way (14).

22 Given these facts, the presented study aimed to answer the question, how do entry design
23 parameters influence safety on Czech roundabouts? Driving behavior on roundabout entries is
24 likely to be influenced by driving path geometry, sight conditions, etc.; however, their impact
25 has not been specifically quantified. The objective was to investigate the relationships between
26 entry design parameters and safety, and if possible, use the findings to update current Czech
27 roundabout design guidelines.

28

29 BACKGROUND

30 International perception of superior roundabout safety performance comes mostly from studies
31 of crash reductions after converting traditional intersections to roundabouts. For example, a
32 study of 23 conversions in the US (15) found 40% reduction of all crashes, 80% of injury
33 crashes, and 90% of fatal crashes. Meta-analysis of 28 studies outside of the US (16) showed
34 30% to 50% reduction in the number of injury crashes; fatal crashes were reduced by 50% to
35 70%. A Czech before-after study (12) identified approx. 50% reduction of both total and injury
36 crashes. And recent meta-regression analysis (17), based on 44 international studies, concluded
37 that converting intersections to roundabouts is associated with a reduction of fatal and injury
38 crashes of about 65% and 40%, respectively.

39 However, roundabout implementations may be influenced by other considerations, such
40 as capacity requirements or spatial constraints; as a result, final performance may not be as safe
41 as expected. When studying roundabout crash types, the highest percentage usually relates to
42 roundabout entries. In a US study, entering-circulating crashes were found to represent about
43 three quarters of all collisions (18); above-average numbers were also identified in samples
44 from the United Kingdom (19: up to 71%) and Switzerland (8: 57%).

45 In terms of roundabout geometry, scientific literature provides indications of several
46 safety-relevant characteristics. Some of them are as follows (sorted chronologically):

- 1 • UK study of 4-leg roundabouts (19) reported several safety-related geometric variables,
2 including entry path curvature, entry path radius (the inverse of entry path curvature)
3 and entry width.
- 4 • According to German experience (20), sufficiently large Δ parameter (defined as the
5 distance between the straightest line from an entry to the opposite exit and the shortest
6 track a driver could take on the circulating roadway) is the precondition to necessary
7 speed reduction. Similar concept was referred to as “lateral displacement” (21) or
8 “lateral deflection” (22).
- 9 • Approach curvature, central island diameter, separation between legs and other factors
10 were found influential in an Australian study (23).
- 11 • Swiss research (8) found correlation between smaller deviation angles and higher crash
12 rates, caused by failing to give way and increased through-speeds.
- 13 • International comparison of roundabout design guidelines (24) concluded that the main
14 roundabout safety determinant is a combination of entry deflection and entry width.
- 15 • A detailed study of roundabout crash contributory factors (14) stressed the crucial role
16 of a moderate radius of deflection and a large deviation angle.

17 In principle, most all the mentioned parameters are related to deflection, either on entries (entry
18 angle, i.e., the conflict angle between the entering and the circulating traffic) or in the
19 roundabout center (deviation angle, i.e., the amount of trajectory change imposed by central
20 island). According to Rodegerdts et al. (7), reducing the vehicle path radius at the entry (i.e.,
21 deflecting the vehicle path) decreases the relative speed between entering and circulating
22 vehicles and thus results in lower entering-circulating vehicle crash rates. These facts have been
23 reflected in several guidelines and standards, for example:

- 24 • Spanish standards (25) set range of entry angle values $20^\circ - 60^\circ$ (ideally 30°); the same
25 range is required by UK *Design Manual for Roads and Bridges* (26).
- 26 • Swiss and Italian standards require a deviation angle above 45° (27, 28).

27 Regarding safety requirements, Czech guidelines recommend verification of through-speeds;
28 however, they do not present any specific values of entry angle or deviation angle. This study
29 aims to fill this gap by investigating the relationships between entry design parameters and
30 safety, and using the findings to update current Czech roundabout design guidelines.

31 To this end, the study comprised three analyses, which are described in the following text.

32 ANALYSES

33 Sound research might provide meaningful insight to improve geometric design standards and
34 guide towards the optimal balance between the conflicting design parameters (28). In order to
35 take into account the multi-factor character of the issue, the first step is a multivariate analysis,
36 which considers simultaneously the effects of many factors on the incidence of crashes (29).
37 Suitable tool for this task is a mathematical equation representing the number of crashes as a
38 function of the explanatory variables (potential risk factors). These equations are referred to as
39 crash prediction models (or safety performance functions, SPFs). In case of roundabouts, SPFs
40 may be of two kinds (30):

- 41 • *Intersection-level* SPFs relate the crash prediction to AADT and possibly other context
42 variables, such as number of lanes or number of legs.
- 43 • *Approach-level* SPFs relate common types of crashes (e.g., approaching, entering-
44 circulating, or exiting-circulating crashes) to specific AADTs and key geometric
45 parameters (risk factors).

1 Analysis 1 – Safety performance functions

2 *Review*

3 Developing SPFs, as a tool of quantitative road safety management, is not a new activity.
4 However, SPFs are usually defined for typical network elements (road segments and
5 intersections). Many countries do not use any specific roundabout SPFs. For example in the
6 US, although a number of roundabout SPFs were developed under NCHRP Project 3-65 (30).
7 none of them was introduced in the current edition of *Highway Safety Manual* (HSM; 31). The
8 on-going NCHRP Project 17-70 aims to develop roundabout SPFs to be used in the second
9 edition of HSM (32).

10 On the contrary, in New Zealand, with long tradition both in roundabout constructions
11 and using SPFs, approach-level SPFs are firmly established and implemented in national
12 evaluation guidelines (33). Also Nordic countries (Denmark, Sweden, Finland) are all using
13 specific roundabout SPFs (34 – 36); however only on the intersection level. In the Czech
14 Republic, roundabout SPFs were developed as well (37 – 39); however no Czech approach-
15 level SPF exists.

16 *Data*

17 Given availability of traffic census (AADT) data on all legs, sample of 200 typical
18 (unsignalized) roundabouts was selected for analysis. In order to study individual entries, each
19 roundabout was split into individual leg segments.

20 Crash data were retrieved from 8 years (2009 – 2016), in a distance of 100m from the
21 roundabout center (approx. 300 ft, based on 40). In the Czech Republic, crash reporting is not
22 routinely linked to specific types, such as entering-circulating crashes; therefore all crash types
23 were used. Regarding their severity, approx. 77% were property-damage-only (PDO) crashes.
24 Distinguishing individual severity levels would thus result in small samples. Therefore,
25 alternative approach was tested: using national values of crash costs for severity levels (41),
26 equivalent of PDO crashes (EPDO) was calculated (value 1 represents one PDO crash, and
27 values 3.68, 32.70, 97.38 represent one slight, severe and fatal injury, respectively). In the
28 analysis, both crash frequency and EPDO were used as a response variable.

29 As mentioned, AADT from national traffic census was used as a source of traffic volume
30 data. This data however do not provide disaggregation into specific movements, such as
31 entering, circulating, or exiting AADT.

32 Road and geometric characteristics were collected from online maps. During collection,
33 it was found that conditions were changing during the 8-year period: there were cases, when
34 for example, a bypass, pedestrian crossing, or even another roundabout leg was added.
35 Therefore, each year was considered individually. AADT values were interpolated between
36 years, according to national traffic forecasting guidelines (42); also EPDO was calculated
37 separately for each year.

38 In a sum, the sample of 200 roundabouts comprised 781 approaches, separated into 8
39 annual records. After some data reduction, these resulted in a total of 5,193 data records. Based
40 on literature review, following road and geometric variables were assigned to all the records:

- 41 • Intersection-level characteristics
 - 42 ○ Location (rural or urban)
 - 43 ○ Roundabout type (single-lane, double-lane, mini, turbo, grade separated)
 - 44 ○ Circular shape (no/yes)

- 1 ○ Number of legs (3, 4, 5 or 6 legs)
- 2 ○ Inscribed circle and central island diameter
- 3 ○ Standard deviation of angles between legs (in case of perpendicular legs, standard
- 4 deviation is zero; the variable shows the difference from the ideal configuration)
- 5 ○ Number of circulatory lanes (1 or 2)
- 6 ○ Circulatory lane width
- 7 ○ Truck apron width
- 8 • Approach-level characteristics
 - 9 ○ Entry angle, Deviation angle, Exit angle (as previously defined)
 - 10 ○ Entry width, Exit width, Bypass width
 - 11 ○ Close proximity features (binary variables showing presence of public transport
 - 12 stop, parking, accesses or intersections, within 100m from roundabout)
 - 13 ○ Number of entry lanes and Number of exit lanes
 - 14 ○ Pedestrian crossing (no/yes)
 - 15 ○ Driving directions (entry, exit or both)
 - 16 ○ Alignment offset (offset of leg alignment from the radial direction)
 - 17 ○ Collision distance (distance between entry and following exit)

18 *Exploratory analysis*







19 The next step was exploratory analysis. During trials, it was found that categorization of some
 20 continuous variables improved their relationship to crash frequency. Therefore, selected
 21 variables were transformed as follows:

- 22 • Entry angle was categorized into 5 intervals: < 20°, (20°; 40°), (40°; 60°), (60°; 80°),
 23 and > 80°.
- 24 • Bypass width, Truck apron width, and Alignment offset were transformed into binary
 25 absence/presence (no/yes).
- 26 • Instead of entry width, variable Entry type was created, using number of entry lanes and
 27 number of circulatory lanes:
 - 28 ○ E1 ... 1 entry lane and 1 circulatory lane
 - 29 ○ E2 ... 1 entry lane and 2 circulatory lanes
 - 30 ○ E3 ... 2 entry lanes and 2 circulatory lanes

31 Next, correlations between all pairs of variables were checked. In case, when correlation
 32 coefficient exceeded 0.5 threshold, one of variables was removed. After these initial steps, 19
 33 remaining variables were prepared for modeling. Table 1 summarizes this selection process.

34

1 **TABLE 1 List of Variables, Transformations and Selection for Modeling**

| | Variable | Transformation | Inter-colleration | Modeling input | |
|---|----------------------------------|-------------------------|--|--|--------------------------------|
| Intersection-level characteristics | Location | | | Location | |
| | Roundabout type | | | Roundabout type | |
| | Circular shape | | | Circular shape | |
| | # legs | |  | | |
| | Inscribed circle diameter | | | Inscribed circle diameter | |
| | Central island diameter | |  | | |
| | Std. dev. of angles between legs | | | Std. dev. of angles between legs | |
| | # circulatory lanes | | | # circulatory lanes | |
| | Circulatory lane width | Entry type categories |  | | |
| | Truck apron width | Apron presence | | Apron presence | |
| Approach-level characteristics | Entry angle | Entry angle intervals | | Entry angle intervals | |
| | Angles | Deviation angle |  | | |
| | | Exit angle | | | |
| | Widths | Entry width | Entry type categories |  | |
| | | Exit width | Entry type categories | | |
| | | Bypass width | Bypass presence | | Bypass presence |
| | Close proximity features | Public transport stop | | | Public transport stop |
| | | Parking | | | Parking |
| | | Access | | | Access |
| | | Different location | | | Different location |
| | | Close intersection type | | | Close intersection type |
| | Other | Number of entry lanes | | | Number of entry lanes |
| | | Number of exit lanes | | | Number of exit lanes |
| Pedestrian crossing | | | | Pedestrian crossing | |
| Driving directions | | |  | | |
| Alignment offset | | Offset presence | | | |
| Collision distance | | | | Collision distance | |

2 Table 2 summarizes descriptive characteristics of this data.

1 **TABLE 2 Descriptive Characteristics of Continuous and Categorical Variables**

| Continuous variables | Min. | Max. | Mean | Std. Dev. |
|--------------------------------------|-------------------------|-----------------------|------------------------|-------------------------|
| Crash frequency | 0 | 16 | 0.47 | 1.14 |
| Crash severity (EPDO) | 0 | 113.42 | 0.83 | 3.60 |
| AADT [veh/day] | 5 | 24520 | 4541.04 | 2813.22 |
| Collision distance [m] | 0 | 106 | 16.90 | 10.87 |
| Inscribed circle diameter [m] | 19 | 139 | 42.20 | 21.44 |
| Std. dev. of angles between legs [°] | 0 | 61 | 15.48 | 11.60 |
| Categorical variables | | | | |
| Access | | <i>no</i> | <i>yes</i> | |
| | | | 42.1% | 57.9% |
| Apron presence | | <i>no</i> | <i>yes</i> | |
| | | | 21.3% | 78.7% |
| Bypass presence | | <i>no</i> | <i>yes</i> | |
| | | | 93.0% | 7.0% |
| Circular shape | | <i>no</i> | <i>yes</i> | |
| | | | 4.7% | 95.3% |
| Close intersection type | <i>X</i> | <i>T</i> | <i>Y</i> | <i>staggered</i> |
| | 18.2% | 60.5% | 3.2% | 1.8% |
| | <i>star</i> | <i>roundabout</i> | <i>grade-separated</i> | <i>none</i> |
| | 0.5% | 8.9% | 4.4% | 2.4% |
| Different location | | | <i>rural</i> | <i>urban</i> |
| | | | 21.1% | 78.9% |
| Entry angle | <i>(0°; 20°)</i> | <i>(20°; 40°)</i> | <i>(40°; 60°)</i> | <i>(60°; 80°)</i> |
| | 14.4% | 47.2% | 33.6% | 3.5% |
| | | | | <i>none (exit only)</i> |
| | | | | 1.3% |
| Entry type | <i>none (exit only)</i> | <i>E1</i> | <i>E2</i> | <i>E3</i> |
| | 1.2% | 88.1% | 5.5% | 5.2% |
| Location | | | <i>rural</i> | <i>urban</i> |
| | | | 20.7% | 79.3% |
| Number of circulatory lanes | | | <i>1</i> | <i>2</i> |
| | | | 90.5% | 9.5% |
| Number of entry lanes | | <i>0 (exit only)</i> | <i>1</i> | <i>2</i> |
| | | 1.3% | 94.4% | 4.3% |
| Number of exit lanes | | <i>0 (entry only)</i> | <i>1</i> | <i>2</i> |
| | | 1.0% | 95.4% | 3.6% |
| Parking | | | <i>no</i> | <i>yes</i> |
| | | | 84.2% | 15.8% |
| Pedestrian crossing | | | <i>no</i> | <i>yes</i> |
| | | | 39.1% | 60.9% |
| Public transport stop | | | <i>no</i> | <i>yes</i> |
| | | | 85.1% | 14.9% |
| Roundabout type | <i>single-lane</i> | <i>double-lane</i> | <i>mini</i> | <i>turbo</i> |
| | 88.5% | 8.4% | 2.0% | 0.7% |
| | | | | <i>grade-separated</i> |
| | | | | 0.4% |

2 *Modeling*

3 Reported data was used to develop SPFs. Consistently with literature (e.g., 19), the basic form
4 comprised only exposure (*AADT*), with further explanatory variables (x_i) being added stepwise,
5 keeping only the ones with achieved statistical significance below 5 %:

$$6 \quad \hat{N} = \exp(\beta_0) \cdot (AADT)^{\beta_1} \cdot \exp(\sum_{i=2}^n (\beta_i \cdot x_i)) \quad (1)$$

7
8

1 where:

2 \widehat{N} ... expected annual crash frequency or crash severity (EPDO)

3 $AADT$... exposure variable (daily traffic volume)

4 x_i ... other explanatory variables (risk factors)

5 β_i ... regression coefficients, to be estimated in modeling

6 Generalized linear modeling procedure in IBM SPSS was applied, using a negative binomial
7 error structure with a logarithmic link function; $AADT$ thus took form of natural logarithm
8 $\ln(AADT)$. The linearized model form is shown in Eq. 2:

$$9 \quad \ln(\widehat{N}) = \beta_0 + \beta_1 \cdot \ln(AADT) + \sum_{i=2}^n (\beta_i \cdot x_i) \quad (2)$$

10 Results

11 During modeling, several insignificant variables were discarded. Table 3 reports parameters of
12 final SPFs (crash frequency SPF and crash severity SPF): regression coefficients β_i and
13 achieved levels of statistical significance (*Sig.*). Statistical significance was below 5% in most
14 cases, with 2 exceptions (in bold), which had levels between 5% and 10%.

15 **TABLE 3 Parameter of Crash Frequency SPF and Crash Severity (EPDO) SPF**

| Variable | Category | Crash frequency SPF | | Crash severity (EPDO) SPF | |
|----------------------------------|------------|---------------------|-------------|---------------------------|--------------|
| | | β_i | <i>Sig.</i> | β_i | <i>Sig.</i> |
| (Intercept β_0) | | -2.800 | 0.000 | -2.940 | 0.000 |
| $\ln(AADT)$ | | 0.583 | 0.000 | 0.583 | 0.000 |
| Collision distance | | -0.005 | 0.012 | -0.009 | 0.014 |
| Std. dev. of angles between legs | | 0.005 | 0.024 | 0.006 | 0.028 |
| Entry angle | < 20° | -0.952 | 0.002 | -0.946 | 0.097 |
| | (20°; 40°) | -1.183 | 0.000 | -1.239 | 0.028 |
| | (40°; 60°) | -1.169 | 0.000 | -1.212 | 0.031 |
| | (60°; 80°) | -1.122 | 0.000 | -1.178 | 0.041 |
| | > 80° | 0 | | 0 | |
| Apron | no | 0.560 | 0.000 | 0.703 | 0.000 |
| | yes | 0 | | 0 | |
| Bypass | no | -0.498 | 0.000 | -0.521 | 0.000 |
| | yes | 0 | | 0 | |
| Entry type | E1 | -1.813 | 0.000 | -1.996 | 0.000 |
| | E2 | -1.123 | 0.000 | -1.277 | 0.000 |
| | E3 | 0 | | 0 | |
| Location | rural | | | 0.188 | 0.017 |
| | urban | | | 0 | |
| Pedestrian crossing | no | | | -0.133 | 0.068 |
| | yes | | | 0 | |

16

1 *Interpretation*

2 Regression coefficients in Table 3 are consistent between Crash frequency SPF and Crash
3 severity (EPDO) SPF. Using the latter enabled identifying also the influence of Location and
4 Pedestrian crossing, which were not statistically significant in the former SPF.

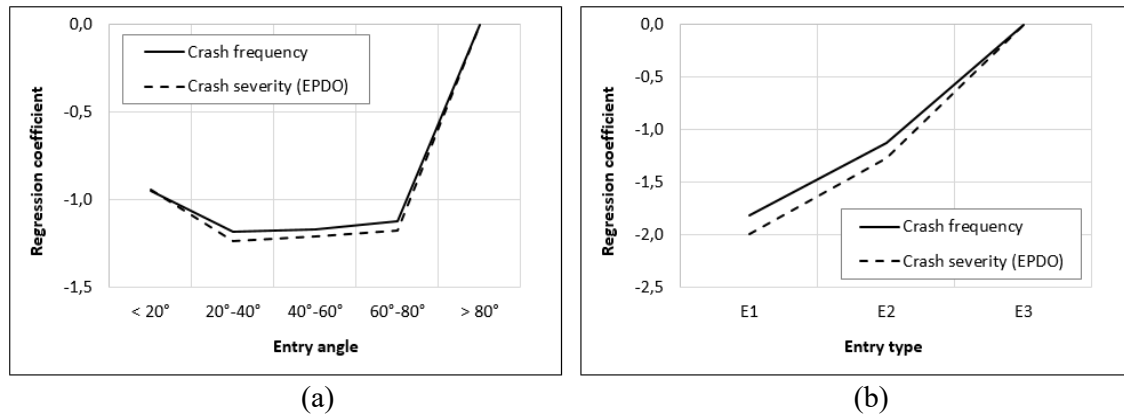
5 Signs of regression coefficients β_i enable interpreting directions of influence of
6 individual variables on response variable:

- 7 • Positive relationship means that change of a variable is associated with change of
8 response variable in the same direction. Therefore, increasing variable increases crash
9 frequency/severity, and decrease of variable decreases crash frequency/severity.
- 10 • Negative relationship that change of a variable is associated with change of response
11 variable in the opposite direction. Therefore, increasing variable decreases crash
12 frequency/severity, and decrease of variable increases crash frequency/severity.

13 Effects of categorical variables are to be interpreted in comparison to the reference category
14 (i.e., the one with zero regression coefficient). For example, missing pedestrian crossing (“no”)
15 has a negative coefficient, thus it is associated with lower crash frequency, compared to the
16 reference category with pedestrian crossing (“yes”).

17 According to Table 3, the variables had following directions of influence:

- 18 • AADT has a positive influence as expected. In addition, coefficient 0.583 is close to
19 values 0.576 from previous Czech SPF (39) or 0.58 from New Zealand SPF (33, Table
20 15).
- 21 • Collision distance has a negative association: the longer distance, the more space for
22 potential evasive manoeuvres and lower crash frequency/severity. This was confirmed
23 also by Maycock & Hall (19) or Arndt (23).
- 24 • Standard deviation of angles between legs has a positive relationship (the more
25 dispersion, the more complex environment and higher crash frequency/severity),
26 consistently with Czech design standards. Also Jensen (43) noted that “as the difference
27 between the smallest and largest angle between arms in a roundabout becomes smaller,
28 the level of safety becomes better.”
- 29 • Regression coefficients for entry angle are displayed in Fig. 1a. The curve has minimum
30 values between 20° and 80°. This is relatively consistent Spanish and British standards,
31 which recommend interval of entry angles 20° – 60° (25, 26).
- 32 • Fig. 1b provides analogical graph for entry types. The trend is rising from E1 (single
33 entry and circulatory lane) to E3 (two entry and circulatory lanes). Positive association
34 between entry width (number of lanes) and crash frequency was identified in several
35 studies (19, 9, 44, 37, 45).
- 36 • Truck apron has a protective influence: its presence is associated with lower crash
37 frequency/severity. This was also confirmed by Šenk & Ambros (37).
- 38 • On the contrary, bypass presence is associated with higher crash frequency/severity.
39 This is probably due to adding another conflict point, which increases crash risk and
40 severity, as noted by Robinson et al. (9) or Daniels et al. (46).
- 41 • Location in rural areas seems to increase crash severity, compared to urban roundabouts;
42 the same holds for presence of pedestrian crossing. Both variables are likely to be
43 associated with speed and vulnerability, as also reported by Turner et al. (44) or Šenk
44 & Ambros (37).



1
2
3 **FIGURE 1 Regression coefficients for categories of (a) entry angle and (b) entry type.**

4 “Location” variable is likely to be a proxy for speed, which was not considered in SPF. In this
5 regards, it would be interesting to measure speed and use it in modeling. Therefore, alternative
6 approach was used for the second analysis step: speeds were measured on a sub-sample of
7 roundabouts and used to explore its relationship to roundabout geometry.

8
9 **Analysis 2 – Speed**

10 *Review*

11 Traditionally, speed measurement has been performed using stationary devices. For example,
12 Rodegerdts et al. (30) used speed gun to measure free-flow speeds in specific points of through-
13 pass trajectory; similar approach was used also by Spacek (8), Turner et al. (44) or Kim & Choi
14 (47). In addition to speed guns, some (48, 49) measured speeds of isolated vehicles also by
15 video camera. However, with these methods speeds are collected only in limited spots.
16 Therefore, alternative methods used video detection or image processing to obtain complete
17 speed profiles (50 – 52). Other studies used speed data collected by car-following (“car-chase
18 method”, mentioned in 21, or “floating vehicle”, 53) or by instrumented vehicles (e.g., 54).

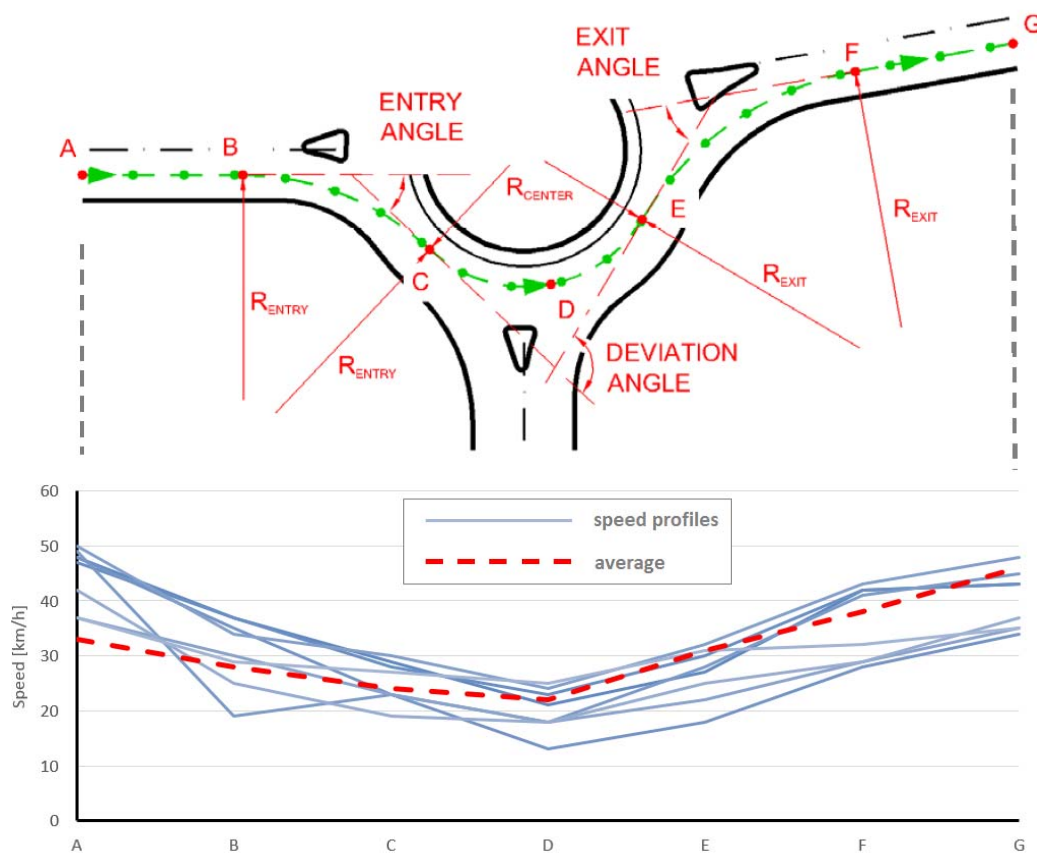
19 *Data*

20 In this study, instrumented vehicle of CDV – Transport Research Centre was used. It is a
21 common van, equipped by data collection sensors (GPS, accelerometers, gyroscopes, video
22 camera). GPS location was operating at 10 Hz frequency (10 records per second), with
23 horizontal precision of 1 meter. It was used to obtain data points, representing vehicle path and
24 continuous speed. Data were collected on a sub-sample of 11 roundabouts, where two drivers
25 passed several times through each leg, totaling 92 through-drives from one leg to the opposite
26 one. Driving was conducted in free-flow conditions (morning and evening off-peak periods).

27 Collected data were processed to obtain relevant radii and angles, distinguish tangent
28 and curve segments and estimate respective speeds. The obtained parameters were:

- 29
- Radii on entry, center and exit
 - Entry angle, deviation angle, exit angle
 - Speeds in seven profiles (A to G):
 - 32 ○ A ... on approach leg (50m upstream of entry)
 - 33 ○ 5 profiles at a roundabout (B, C, D, E, F)
 - 34 ○ G ... on exit leg (50m downstream of exit)

1 The parameters, together with an example of speed profiles, are displayed in Fig. 2.



2
3
4 **FIGURE 2** Through-pass trajectory parameters and example of speed profiles.

5 *Results*

6 To assess the influence of radii and angles on speed, Spearman correlation coefficients were
7 calculated. Unfortunately, only some exceeded 0.5 threshold, which is perceived as a threshold
8 of moderate correlation (55). These were correlations between:

- 9
- 10 • speed 50m upstream of entry and entry angle
 - 11 • speed 50m upstream of entry and entry radius
 - 12 • speed in center and central radius

13 The first two associations relate to roundabout entries, which indicates their relationship to
14 safety. In the first analysis, link between geometry and safety was established through crash
15 frequency/severity SPFs; the second analysis showed the link between geometry and speed.
16 One may thus anticipate a causal chain: geometry – speed – safety. In order to confirm existence
17 of this chain, the third analysis attempted to develop SPF, which contain both geometry and
18 speed variables.

1 Analysis 3 – Safety performance functions with speed

2 *Review*

3 Several international studies employed speed variables in their SPFs (e.g., 56, 23, 44, 57). On
 4 the other hand, some of them did not succeed, for example NCHRP Project 3-65 (30), where
 5 estimated model was deemed inadequate on the basis of weak effects of speed variables. One
 6 of problems may be the use of different speed definitions, such as speed limits, measured
 7 speeds, predicted/simulated speeds, etc. Other authors attempted estimating speed from
 8 geometric parameters, and then using it to model crash frequencies (58, 49, 59). These studies
 9 differed in using measured or predicted speeds, and in function form of speed (either power or
 10 exponential form). It is thus evident that although developing speed-based SPFs is not a new
 11 task, it is still not a formalized approach.

12 *Data*

13 This analysis was based on previously described data collected at 11 roundabouts. Following
 14 variables were used:

- 15 • crash frequency or crash severity as a response variable, collected for each through-pass
- 16 • angles and radii as explanatory variables
- 17 • speeds in profiles A to G as additional explanatory variables

18 Instead of AADT, hourly traffic flow in respective trajectories, was counted on the site.
 19 Descriptive characteristics of data are reported in Table 4.

20 **TABLE 4 Descriptive Characteristics of Crash, Geometry and Speed Data**

| Variable | Unit | Min. | Max. | Mean | Std. Dev. |
|---------------------|---------|------|-------|--------|-----------|
| Crash frequency | [-] | 1 | 25 | 9.26 | 6.60 |
| EPDO | [-] | 1 | 59.22 | 15.69 | 14.50 |
| Hourly traffic flow | [veh/h] | 64 | 1600 | 548.93 | 488.00 |
| Entry angle | [°] | 2 | 75 | 34.37 | 15.93 |
| Deviation angle | [°] | 40 | 191 | 79.56 | 32.04 |
| Exit angle | [°] | 8 | 52 | 31.48 | 11.73 |
| Entry radius | [m] | 18 | 113 | 36.59 | 18.39 |
| Central radius | [m] | 12 | 28 | 19.67 | 3.81 |
| Exit radius | [m] | 25 | 92 | 38.04 | 13.80 |
| Speed A | [km/h] | 31 | 54 | 42.33 | 6.34 |
| Speed B | [km/h] | 23 | 40 | 31.63 | 4.13 |
| Speed C | [km/h] | 21 | 35 | 26.93 | 3.35 |
| Speed D | [km/h] | 18 | 30 | 24.44 | 2.94 |
| Speed E | [km/h] | 23 | 40 | 31.04 | 3.54 |
| Speed F | [km/h] | 28 | 50 | 38.00 | 4.92 |
| Speed G | [km/h] | 30 | 64 | 44.41 | 8.71 |

21 *Results*

22 The model form described in Equation 1 was used (with hourly traffic flow instead of AADT).
 23 Apart from traffic flow, the SPF introduce entry angle, and speed 50m upstream of entry.
 24 Parameters of developed SPF (regression coefficients β_i and achieved levels of statistical
 25 significance, all below 5%) are reported in Table 5.

26

1 **TABLE 5 SPF Parameters**

| Variable | β_i | Sig. |
|-----------------------------|-----------|-------|
| (Intercept β_0) | 5.211 | 0.022 |
| ln (hourly traffic flow) | -0.727 | 0.007 |
| Entry angle | -0.052 | 0.001 |
| Speed 50m upstream of entry | 0.066 | 0.031 |

2 Typically, AADT has a positive relationship to crash frequency; on the contrary, negative
 3 coefficient of traffic flow was found in all three SPFs. Although not expected, several studies
 4 also had such finding:

- 5 • Satterthwaite (60) found that rear-end crash rates increased with traffic flow, while
 6 single-vehicle rates decreased.
- 7 • Hiselius (61) identified similar confusion, when mixing volumes of cars and trucks.
- 8 • Analysis by Christoforou et al. (62) concluded that low volume (free-flow) conditions
 9 may lead to higher speeds, which in turns cause unexpected direction of traffic flow
 10 influence on safety. The unexpected sign of regression coefficient may be thus due to
 11 using aggregated input data.

12 Signs of other regression coefficients are as expected from literature:

- 13 • Entry angle has a protective effect: the higher angle, the lower speed and risk.
- 14 • Speed on approach has a positive relationship to crashes: increasing speed is associated
 15 to increasing crash frequency.

16 **DISCUSSION AND CONCLUSIONS**

17 The study comprised three analyses: crash-based safety performance functions (SPFs), speed
 18 analysis, and finally SPFs which incorporated speed. The analyses were different in terms of
 19 their data needs: while crash-based SPFs required crashes, traffic volumes and geometry (i.e.,
 20 data that are usually available network-wide), the second and third approach required speed
 21 data, that had to be especially collected. This is why samples were different (200 roundabouts
 22 in Analysis 1 vs. 11 roundabouts in Analyses 2 and 3). On the other hand, using speed in
 23 analyses adds an extra value, since it may be considered a proxy for driving behavior, which is
 24 likely to enhance the quality of developed models.

25 With the aim of investigating the influence of roundabout entry design parameters on
 26 safety, the analyses concluded as follows:

- 27 • Analysis 1 developed approach-level SPFs. Consistently with literature, a number of
 28 variables were significantly related to crashes, including entry angle and entry type.
 29 Using crash severity (EPDO) in addition to crash frequency also enabled revealing
 30 significant influence of location (rural/urban) and presence of pedestrian crossing on
 31 roundabout leg.
- 32 • In analysis 2, speeds were measured on a sub-sample of roundabouts and used to explore
 33 its relationship to roundabout geometry. Correlation was found between approach
 34 speeds (50m upstream of entry) and entry angle and entry radius.
- 35 • Analysis 3 successfully incorporated approach speed into SPF and confirmed that
 36 increasing speed is associated to increasing crash frequency; again it was demonstrated
 37 that entry angle has a protective effect.

38 Thus, it was proved that entry design parameters have a statistically significant influence on
 39 safety, in terms of crash frequency, severity and speeds. The SPF suggested suitable range of

1 entry angle values, which should be considered in Czech roundabout design guidelines TP 135
2 (63). Currently they only recommend a deviation of entry trajectory from entry axis, which may
3 not be sufficient to reach necessary speed reduction of vehicles entering circulatory lane. The
4 analysis also identified the influence of entry radius; at the same, Czech guidelines mention
5 verification of fastest path radii, but without mentioning any specific values of entry or radii.

6 At the same time, the authors are aware of several limitations:

- 7 • Input crash data is likely to be underreported. In addition, routine crash reporting does
8 not allow distinguishing individual crash types.
- 9 • Routinely collected AADT data, which does not consider individual movements, are
10 also not ideal.
- 11 • Through-pass trajectory identification was based on circular elements only, without
12 consideration of transition curves.
- 13 • Speed data was collected only by one instrumented vehicle and two drivers, which may
14 not provide representative speed behavior data. Sample of 11 roundabouts, where
15 speeds were measured, was also small.

16 Further activities should aim to expand sample size and consider the mentioned limitations of
17 crash, AADT and speed data. Nevertheless, the presented results indicate existence of a causal
18 chain: geometry – speed – safety. The study found that:

- 19 1. Both crash frequency and severity is influenced by roundabout entry geometry.
- 20 2. At the same time, the geometry influences driving speeds.
- 21 3. Safety performance is thus dictated by both geometry and speeds.

22 In future, these points may be further elaborated to develop a “two-stage” tool for roundabout
23 safety analysis (49). In its first stage, speed may be modeled based on geometry and used in the
24 second stage as a surrogate safety measure (instead of crash-based measures) to assess safety,
25 even during the planning phase.

26

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35

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